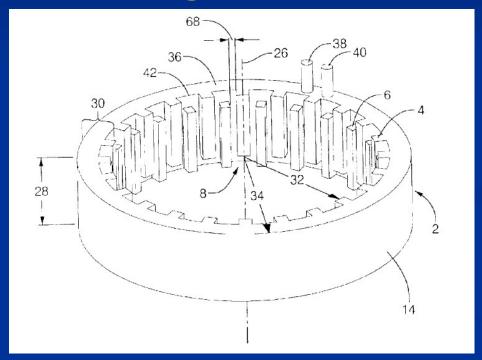
Inteligencia de campo, procedimientos para la búsqueda de patentes y marcas registradas



Dr. Ramón Alberto Sánchez Piña Universidad de Harvard rsanchez@hsph.harvard.edu

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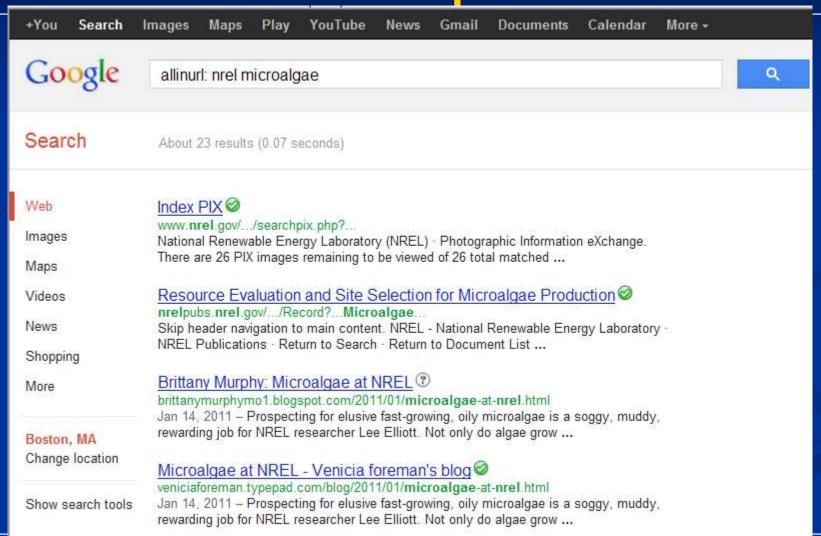
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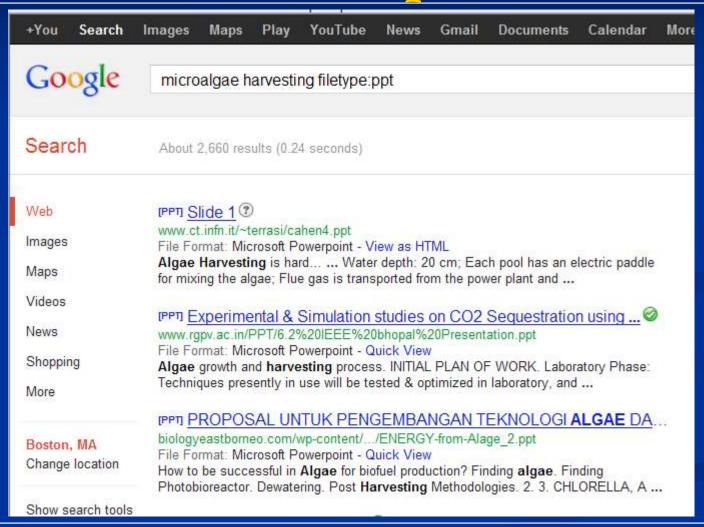
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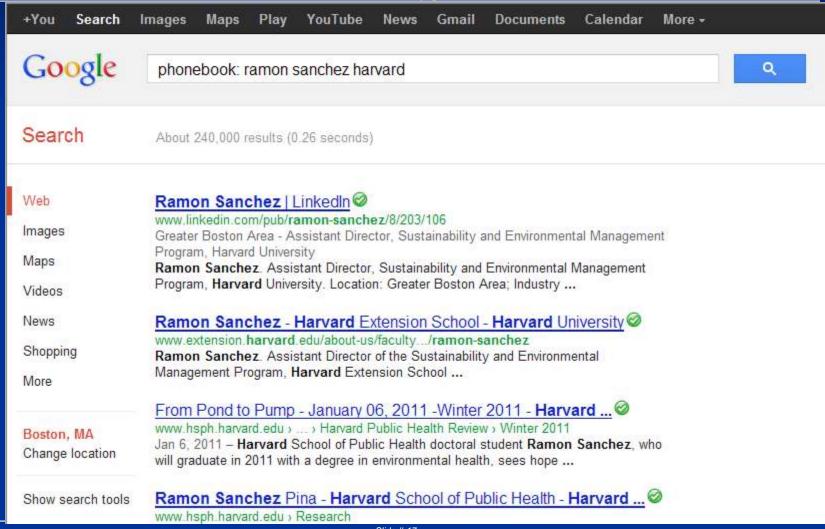
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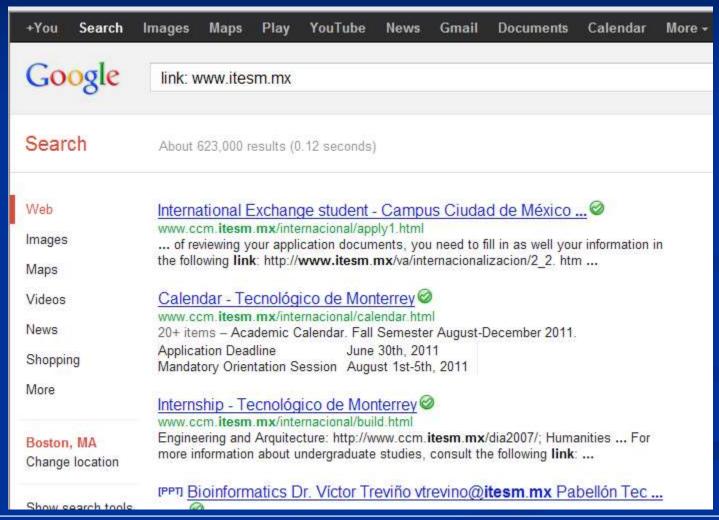
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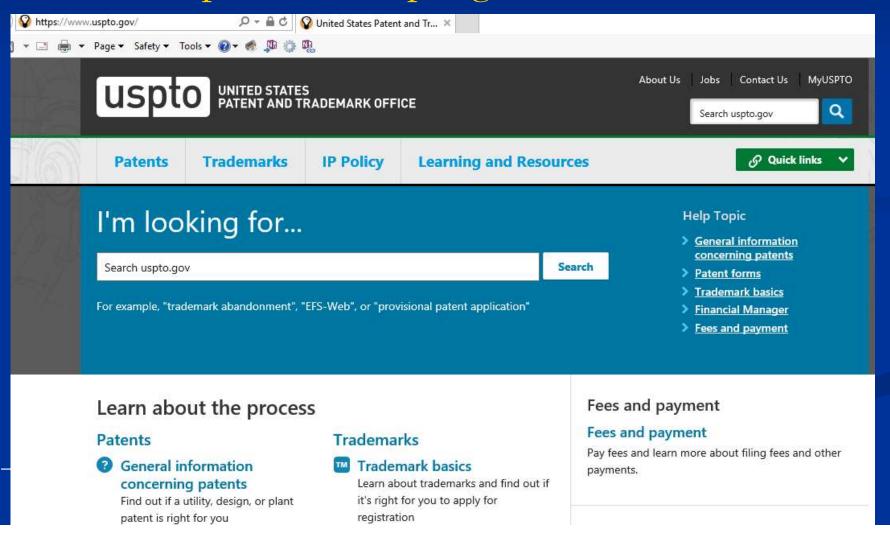


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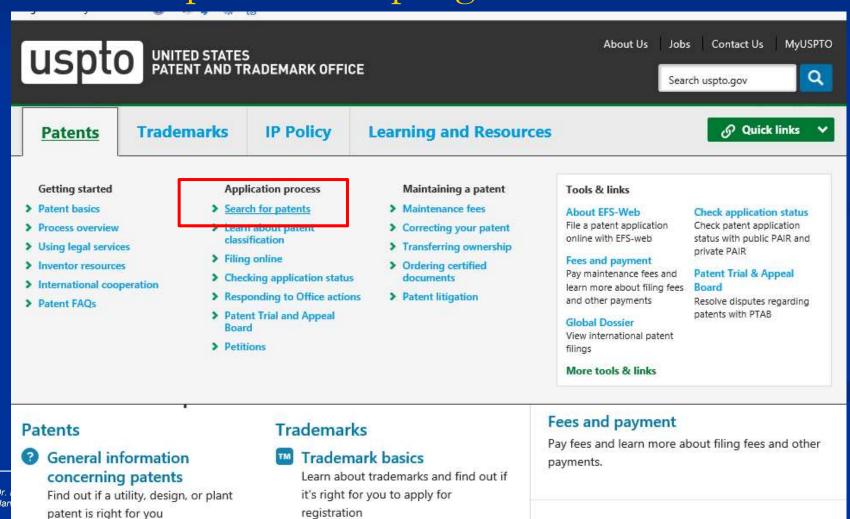
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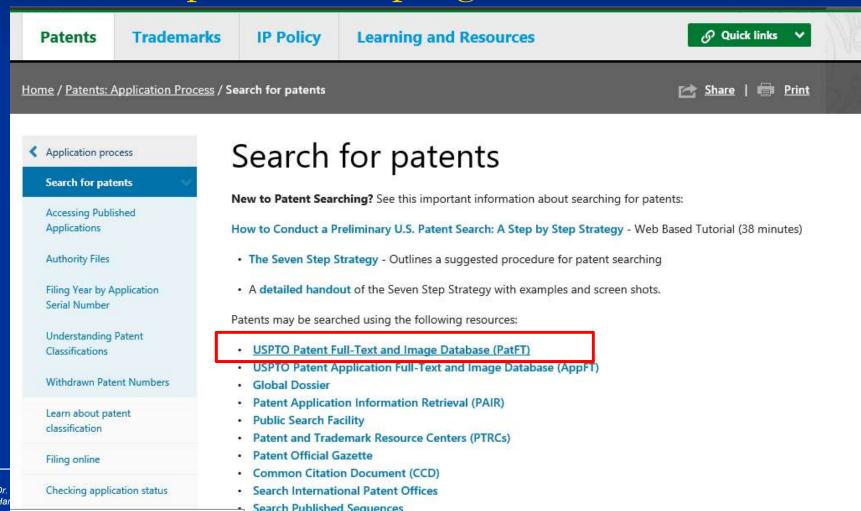
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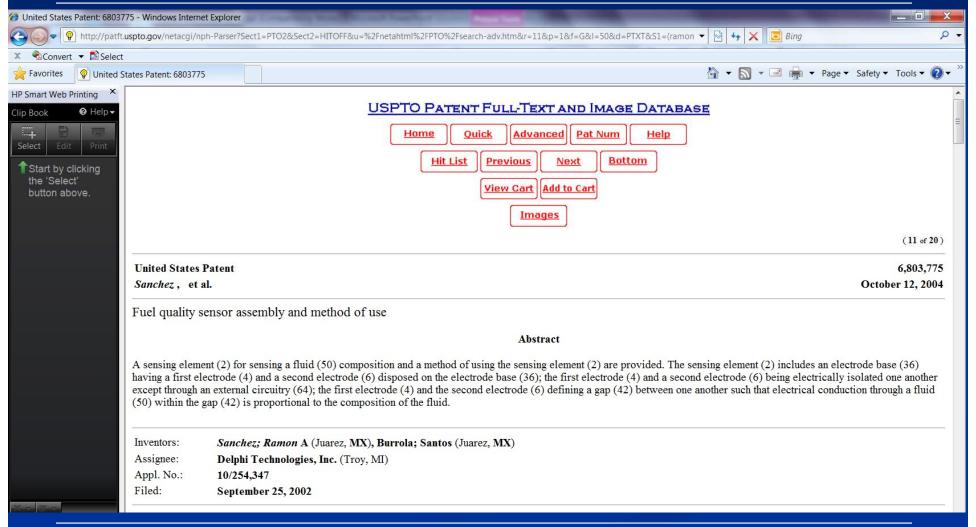
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| 7 20040055371 | PACKAGING FOR RF SIGNAL SENSOR WITH BATTERY CHANGING CAPABILITIES AND METHOD OF USING |
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(12) United States Patent

Sanchez et al.

US 6,803,775 B2 (10) Patent No.: (45) Date of Patent: Oct. 12, 2004

| (54) | FUEL QUALITY | SENSOR | ASSEMBLY AND | |
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| | METHOD OF US | E | | |

(75) Inventors: Ramon A Sanchez, Juarez (MX); Santos Burrola, Juarez (MX)

(73) Assignce: Delphi Technologies, Inc., Troy, MI

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 40 days.

(21) Appl. No.: 10/254,347

(22) Filed: Sep. 25, 2002

Prior Publication Data US 2004/0056670 A1 Mar. 25, 2004

(51) Int. Cl.7 G01R 27/08; G01R 31/08; 324/698; 324/724; 324/515; 73/861.15

(58) Field of Search 324/698, 722, 324/515, 695, 664, 693, 691, 724; 123/494, 511; 73/861.15, 53.05

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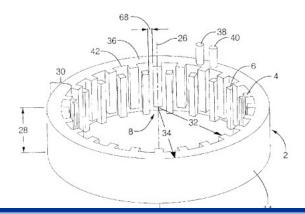
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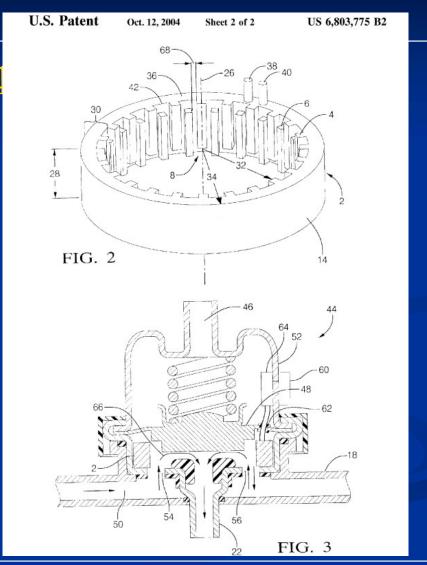
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Primary Examiner-Anjan K. Deb (74) Attorney, Agent, or Firm-Jimmy L. Funkc

A sensing element (2) for sensing a fluid (50) composition and a method of using the sensing element (2) are provided. The sensing element (2) includes an electrode base (36) having a first electrode (4) and a second electrode (6) disposed on the electrode base (36); the first electrode (4) and a second electrode (6) being electrically isolated one another except through an external circuitry (64); the first electrode (4) and the second electrode (6) defining a gap (42) between one another such that electrical conduction through a fluid (50) within the gap (42) is proportional to the composition of the fluid.

29 Claims, 2 Drawing Sheets





US 6,803,775 B2

2

FUEL QUALITY SENSOR ASSEMBLY AND METHOD OF USE

BACKGROUND

Fuel used in internal combustion engines is typically contained in a tank or reservoir as a mixture. Depending on the source of the fuel, it may comprise one or more different fuel components in an unknown ratio. Automobile fuel, for example may be gasoline, including any of its variant blends of aliphatic, olefinic, and/or aromatic hydrocarbons. It may further include various alcohols such as methanol, ethanol, propanol, butanol, pentanol, octanol, and the like. Other components that may be present include octane improvers such as methyl tetriar's buttyl ether (MTBE) and the like.

Each of these fuel components requires different parameters for optimal combustion. These parameters include specific air to fuel ratios, spark plug timing, injector volume, and the like. When the precise composition of the fuel is unknown, or is ever-changing, accurate determination of the optimal combustion parameters depends on being able to quickly and accurately sense fuel mixture composition and other parameters indicative of optimal end use parameters. One approach to optimal engine operation requires the ability to sense characteristics of the fuel, and adjust the operational conditions of the engine accordingly.

Systems have been designed to sense the characteristics of various blends of fuels, such as gasoline and methanol. U.S. Pat. No. 4,48,87,49 to Schwippert is directed to an optical sensor that uses the overall refractive index of the fuel as an indication of composition. Aromatic content of the fuel as an indication of the optical sensor elements over time can result in variations of refractive index that lead to inaccuracy in the

Microwave fuel composition sensors utilize the fuels overall dielectric constant through microwave attenuation. Besides adding significant cost, these sensors operate at extremely high frequencies (e.g., 1–30 Giga Hertz) and generate amounts of electromagnetic noise that can interfere with other electronic components.

Sensors, which utilize the fuel mixture as a dielectric in a capacitive cell, are also capable of correlating the dielectric constant of a fuel mixture to its composition. These sensors have the benefit of being rupped and can be designed for a used in environments in which other sensors would be unacceptable. Unfortunately, the conductivity of various fuel mixtures varies in a non-linear relationship depending on component concentrations. This phenomena is made worse by impurities, especially water. These sensors also need to be made relatively large as compared to other sensors to achieve the level of sensitivity required to sense fuel in an efficient manner. Space and size limitations imposed by design, and the need to minimize void volume in fuel delivery systems, among other factors, have limited the usefulness of capacitive fuel sensors in automotive fuel delivery system applications. A rugged, compact sensor having a sensitivity capable of discriminating between a wide range of fuel blends would be beneficial to optimal combustion of fuel, especially in an internal combustion 60

SUMMARY

Described herein is a sensing element for measuring a fluid composition comprising: an electrode base having a 65 first electrode and a second electrode disposed thereon; the first electrode and said second electrode being electrically

isolated from one another; said first electrode and said second electrode being configured, dimensioned, and positioned to define a gap therebetween such that electrical conduction through the fluid within said gap is proportional to the composition of said fluid.

Also disclosed is a method of sensing a fluid composition comprising: contacting said fluid composition with a sensing element in communication with a circuitry, said sensing element comprising: an electrode base having a first electrode and a second electrode disposed thereon; said first electrode and said second electrode being electrically isolated from one another, except through said circuitry; said first electrode and said second electrode being configured, dimensioned, and positioned to define a gap therebetween 15 such that electrical conduction through a fluid within said gap is proportional to the composition of said fluid; a first electrical connector to provide electrical communication between said first electrode and said circuitry; and a second electrical connector to provide electrical communication between said second electrode and said circuitry; determin ing said electrical conduction of said fluid; and correlating said electrical conduction to said fluid composition.

Further disclosed herein is a combined fluid pressure regulator and assembly for sensing a fluid composition, comprising: a sensing element disposed within a fluid flow path located within a fluid pressure regulator housing; said sensing element comprising: an electrode base having a first electrode and a second electrode disposed thereon; said first electrode and said second electrode being electrically isolated from one another except through an external circuitry; said electrode base having an inner surface and an outer surface separated by a thickness; said outer surface being continuously disposed around a central axis to form an essentially cylindrical shape; said electrode base defining a flow path parallel to said central axis having a flow path length; said first electrode being a plurality of first electrode teeth disposed on said inner surface depending away from said outer surface towards said central axis; said second electrode being a plurality of second electrode teeth on said inner surface depending away from said outer surface towards said central axis: said first electrode teeth and said second electrode teeth being configured, dimensioned, and positioned in a substantially alternating pattern to define a plurality of gaps therebetween such that electrical conduction through a fluid within said plurality of gaps is proportional to a composition of said fluid; said fluid pressure regulator housing comprising a first fluid conduit and a second fluid conduit which allows said fluid to travel through said fluid flow path located with said fluid pressure regulator housing; a regulator valve mounted therein responsive to a fluid demand and disposed in sealing commun tion between said first conduit and a bypass conduit; a first electrical connector being channeled through a sealing member disposed in said regulator valve to provide electrical communication between said first electrode and said external circuitry; and a second electrical connector being channeled through a sealing member disposed in said regulator valve to provide electrical communication between said second electrode and said external circuitry

The above described and other features are exemplified by the following figures and detailed description.

DRAWINGS

Referring now to the figures wherein like elements are umbered alike:

FIG. 1 shows a combustion engine having a fuel compoition sensor;

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another to form a single first electrode. Also, the structures that form the second electrode teeth 6 are all preferably in electrical contact with one another to form a single second electrode. First and second electrodal connectors 38 and 40 provide electrical conductivity between the electrodes and external circuitry. Both of which are in electrical contact with their respective electrodes 4 and 6, but are electrically isolated from each other. The multiple teeth or other such structures serve to increase the available surface area available for sensing given the total size of the sensing element. This is important because the overall sensitivity of the sensing element increases as the available surface area

The value of the outer dimension 34, the inner dimension 32, and the fluid passage length 28 depend on the characteristics required of the sensor element 2. Each of these two electrodes also has an associated total surface area. By defining the total surface area of the electrodes as being the underlying geometric surface area (e.g., for a rectangle, base multiplied by height), the total surface area of the first electrode, when the sensor is used, for example, in a fuel delivery system, is greater than or equal to about 50 square millimeters (mm²) Preferably within this range, the total surface area of the first electrode is greater than or equal to about 30, more preferably greater than or equal to about 30 mm² as represented by the underlying geometric area.

Also, by defining the total surface area of the first electrode as being equal to unity (i.e., equal to one), the proportion of the total surface area of the first electrode to the total surface area of the first electrode to the total surface area of the second electrode determined in the same way is a ratio of about 1 to 0.01, to a ratio of about 1 to 0.00. Preferably within this range, the proportion of total surface areas of the first electrode to the total surface area of the second electrode is a ratio of greater than or equal to about 1 to 0.1, more preferably greater than or equal to about 1 to 0.5. Also within this range, the proportion of total surface areas of the first electrode to the total surface area of the second electrode is a ratio of less than or equal to about 1 to 10, more preferably less than or equal to about 1 to 10, more preferably less than or equal to about 1 to 2, with a ratio of 1:1 being most preferred.

The sensing element is preferably located within a housing to form a sensing assembly 20. The sensing element 2 is
disposed within the housing and arranged such that the fluid
of interest is able to occupy the gaps 42 between the
electrodes and thus be in contact with the sensing element. 45
Preferably, the housing is closed except for a fluid inlet
conduit and a fluid outlet conduit. The housing provides a
conduit or flow path between the inlet an outlet conduits, and
in communication with the sensing element. Preferably, the
fluid is able to enter the housing, contact the sensing element
along the fluid passage length 28, and then exit the housing.

When used to determine the composition of fuel for an internal combustion engine, for example, the sensing assembly is preferably located in close proximity to the point at which the fuel is combusted and also preferably has a total 55 volume that does not interfere with optimal combustion of the fuel.

To prevent extraneous effects between the housing and the sensing element, the shape of the housing is preferably complementary to the shape of the outer surface of the escaining element. As used berein the term complementary is defined as the two being essentially the same. For example, when the outer surface of the sensing element is essentially cylindrical, the housing is thus preferably essentially cylindrical, the housing also has an inner diameter in excess as of the outer diameter of the sensing element to allow fuel to freely flow within the housing.

In the embodiment shown in FIG. 3, the sensing element 2 is disposed within a fuel pressure regulator 44. Within the fuel pressure regulator-bousing 52 is a regulator valve 48 disposed in scaling communication between a fluid rail conduit 18, and a bypass conduit 22. Preferably, the regulator valve 48 is responsive to fluid demand via pneumatic communication with an air intake manifold through manifold conduit 46. In this arrangement, the sensor element 2 is concentrically disposed within, and bounded by the fuel pressure regulator housing 52 and by the regulator valve 48. A fluid conduit or flow path 66 between the fuel rail inlet 54 and the fuel rail outlet 56 is provided by the regulator housing 52 such that the sensing element 2 is located within this flow path 66.

Electrical connection between the sensing element 2 and an external electronic system is preferably provided by directing the electrical connectors 38 and 40 through a seating member 62 located within the regulator valve assembly 44, and preferably to an external electrical connector 60. Also, a portion of and/or all of the necessary electronics may be located as on electronics package 64 within a portion of the bousing 52, depending on space limitations and design needs.

The sensor is in communication with, and preferably electrically connected to an electronic circuitry capable of providing information as to the composition of the fluid the sensor comes in contact with. The electronic circuitry may include a computer or computers capable of using the information derived from the sensor to adjust the combustion parameters of the engine to an optimal value for the fuel mixture flowing through sensor. For this purpose, the computer or computers can include a standard read only memory (ROM) containing a multiple dimensioned lookup table containing compensation factors to be repeatedly looked up with a combination of capacitance and other factors including ambient and engine temperature, exhaust gas composition, ambient air analysis and the like. These compensation factors can be used directly, or can be associated with additional inputs and lookup tables.

While preferred embodiments have been shown and described, various modifications and substitutions may be made thereto without departing from the spirit and scope of the invention. Accordingly, it is to be understood that the apparatus and method have been described by way of illustration only, and such illustrations and embodiments as have been disclosed herein are not to be construed as limiting to the claims.

We claim:

A sensing element for measuring a fluid composition comprising:

an electrode base being disposed about an axis, said electrode base having an inner surface defining an aperture extending through the electrode base for allowing a fluid to flow therethrough; and

a first electrode and a second electrode coupled to said electrode base and electrically isolated from one another, said first electrode having a first plurality of electrode teeth extending radially inwardly from said inner surface of the electrode base into said aperture, and said second electrode having a second plurality of electrode teeth extending radially inwardly from said inner surface into said aperture, said first plurality of electrode teeth being electrically connected together, and said second plurality of electrode teeth being electrically connected together, wherein said second plurality of electrode it electrode teeth being electrically connected together, wherein said second plurality of electrode in a substant

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| Field Code | Field Name | Field Code | Field Name |
|------------|------------------------------|------------|-------------------|
| PN | Patent Number | IN | Inventor Name |
| ISD | Issue Date | IC | Inventor City |
| TTL | <u>Title</u> | IS | Inventor State |
| ABST | Abstract | ICN | Inventor Country |
| ACLM | Claim(s) | LREP | Attorney or Agent |
| SPEC | Description/Specification | AN | Assignee Name |
| CCL | Current US Classification | AC | Assignee City |
| ICL | International Classification | AS | Assignee State |
| APN | Application Serial Number | ACN | Assignee Country |
| APD | Application Date | EXP | Primary Examiner |

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USPTO PATENT FULL-TEXT AND IMAGE DATABASE



(2 of 150)

United States Patent

Keiser, et al.

8,110,163

February 7, 2012

Complexation and removal of heavy metals from flue gas desulfurization systems

Abstract

A method for the reduction of the emission of mercury into the environment from the burning of fossil fuels with the use of polydithiocarbamic compounds. The polydithiocarbamic compounds are used for the capture of mercury from the resulting flue gases using a flue gas desulfrization systems or scrubbers. The method uses polydithiocarbamic compounds in conjunction with a scrubber to capture mercury and reduce its emission and/or re-emission with stack gases. The method is a unique process of reducing the toxic levels of mercury, which allows for the use of *coal as a clean* and environmentally friendlier fuel source.

Inventors: Keiser; Bruce A (Naperville, IL), Shah; Jitendra (Naperville, IL), Sommese; Anthony G. (Aurora, IL), Capener; Lars E. (Aurora, IL), TenEyck; Peter

(Wexford, PA), Wysk; Ralf (Dorsten, DE)

Assignee: Nalco Company (Naperville, IL)

Appl. No.: 11/952,637

Filed: December 7, 2007

(12) United States Patent

(54) COMPLEXATION AND REMOVAL OF HEAVY METALS FROM FLUE GAS DESULFURIZATION SYSTEMS

(75) Inventors: Bruce A Keiser, Naperville, IL (US);
Jitendru Shah, Naperville, IL (US);
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Wysk, Dorsten (DE)

(73) Assignee: Nalco Company, Naperville, IL (US)

(*) Notice: Subject to any disclaimer, the term of this

patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: 11/952,637

(22) Filed: Dec. 7, 2007

(65) Prior Publication Data US 2009/0148372 A1 Jun. 11, 2009

(51) Int. Cl.

210/729, 735, 914
See application file for complete search history.

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No.: US 8.110.163 B2

(45) Date of Patent:

Feb. 7, 2012

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Primary Examiner — Timothy Vanoy (74) Attorney, Agent, or Firm — Edward O. Yonter; Michael B. Martin

57) ABSTRACT

A method for the reduction of the emission of mercury into the environment from the burning of fossil fuels with the use of polydithiocarbamic compounds. The polydithiocarbamic compounds are used for the capture of mercury from the resulting flue gases using a flue gas desulfrization systems or scrubbers. The method uses polydithiocarbamic compounds in conjunction with a scrubber to capture mercury and reduce its emission and/or re-emission with stack gases. The method is a unique process of reducing the toxic levels of mercury, which allows for the use of coal as a clean and environmentally friendlier fuel source.

25 Claims, No Drawings

US 8,110,163 B2

COMPLEXATION AND REMOVAL OF HEAVY METALS FROM FLUE GAS DESULFURIZATION SYSTEMS

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TECHNICAL FIELD

This invention relates to the reduction of the emission of mercury into the environment from the burning of coal and/or other carbon-based fitels. The invention relates to the method of the capture of mercury from flue gases by flue gas desulfurization systems or scrubbers. The invention demonstrates the method of reducing the toxic levels of mercury, which allows for the use of coal as a clean and environmentally friendlier fuel source.

BACKGROUND

The demand for electricity continues to grow globally. In order to keep stride with the growing demand, coal is being looked to as a source for its generation. At present, burning 31 coal produces some 50% of the electricity generated in the United States. The burning of coal in power generation plants results in the release of energy, as well as the production of solid waste such as bottom and fly ash, and flue gas emissions into the environment. Emissions Standards, as articulated in 31 The Clean Air Act Amendments of 1990 as established by the U.S. Environmental Protection Agency (EPA), requires the assessment of hazardous air pollutants from utility power plants.

The primary gas emissions are criteria pollutants (e.g. sulfur dioxide, nitrogen dioxides, particulate material, and carbon monoxide). About two thirds of all sulfur dioxide and a quarter of the nitrogen dioxide in the atmosphere is attributable to electric power generation achieved by burning coal and other fuels.

Secondary emissions depend on the type of coal or fuel being combusted but include as examples mercury, selenium, arsenic, and boron. Coal-fired utility boilers are known to be a major source of anthropogenic mercury emissions in the United States. In December of 2000, the EPA announced their intention to regulate mercury emissions from coal-fired utility boilers despite the fact that a proven best available technology (BAT) did not exist to capture or control the levels of mercury released by the combustion of coal. This has been further complicated by the lack of quick, reliable, continuous monitoring methods for mercury.

The fact remains that mercury is found in coals at concentrations ranging from 0.02 to 1 ppm. The mercury is present as sulfides, or associated with organic matter. Upon combustion the mercury is released and emitted into the flue gas as a gasecus elemental mercury and other mercury compounds. The mercury appears in the flue gas in both the solid and gas phases (particulate-bound mercury and apon-phase mercury, respectively). The so-called solid phase mercury is really vapor-phase mercury adoredo onto the surface of ash and/or of carbon particles. The solid-phase mercury can be captured by existing particle control devices (PCDs) such as electrostatic

precipitators (ESPs) and fabric filters (FF), the latter is sometimes referred to as baghouses.

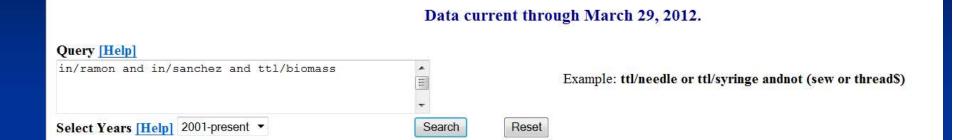
A review of data collected by the EPA in 1999 under the Mercury Information Collection Request (ICR) showed that 5 PCDs alone could capture from 20 to 42% of the total mercury in the fuel. Of course, the efficiency of this strategy depends on the fuel composition, the operating temperature and design of the PCD. Indeed, it has been found that fabric filters tend to exhibit better particulate laden mercury 10 removal, compared to cold-side ESPs, as a result of the formation of filter cake within the filter. The filter cake contains constituents that absorb and/or absorb mercury such as unreacted carbon, activated carbon, iron, and fly ash. As such the filter cake can act as a site to facilitate gas-solid recution 15 between the vapor-phase mercury and the trapped solid particulate. The data suggests FF's can currently achieve as much as 82% mercury capture.

The volatility of mercury and many of its compounds results in a significant portion of the total mercury existing as 20 vapor-phase mercury in the flue gases. Vapor-phase mercury is composed of elemental mercury and oxidized mercury, the relative amounts of these forms being dependent on the amount of chloride in the coal, iron oxide levels in the coal and other constituents in the fly as has examples. Speciation, 25 which refers to the form of vapor-phase mercury, is a key parameter in development and design of capture strategies for mercury emissions. Generally there are two forms of mercury that constitute vapor-phase mercury. The forms are oxidized (fls²⁺ as an example) and elemental (fle²) mercury.

Several control strategies have been developed for the control of mercury emissions from coal-fired boilers. Some of these methods include injection of activated carbon, modified activated carbon, various chemical catalysts, and inorganic sorbents. Unfortunately, none of these strategies removes all the mercury from the flue gas. The efficiencies range from as low as 30% to as high as 80% based on the amount of mercury entering the system with the coal. In addition, these technologies either produce unwanted effects on by-products such as impacting the quality of fly ash, or generate additional waste streams for the power plant. Both lead to higher operational costs for the power plant. One promising strategy is to take advantage of existing air pollution control devices or APCDs to augment or to serve as the primary means to remove vaporphase mercury. Two examples of APCDs are semi-dry and wet scrubbers or Flue Gas Desulfurizer (FGD). Semi-dry FGDs are also known as Spray Dryer Absorbers or SDAs.

Sulfur oxides (SO₂) regulatory compliance mandates the use of at least one of several control strategies. Three such strategies that are used in the US are sorbent injection into the boiler during coal burning and wet or dry Flue Gas Desulfurizes. At present about 3% of the coal-fired power plants are using sorbent injection. FGD scrubbing accounts for 85% using wet and 12% using dry scrubber technologies. Wet scrubbers nichoeve greater than 90% SO₂ removal efficiency compared to 80% by dry scrubbing. In wet scrubbers, the flue gas is brought into contact with slurry containing an alkaline calcium mineral, such as lime or limestone. The SO₂ is adsorbed into the water and reacts to form calcium sulfite. It has been demonstrated that simultaneous to SO₂ capture, wet FGDs can be used to capture vapor-phase mercury from the flue gas.

Elemental mercury is water insoluble and is not removed by a wet FGD. In contrast, oxidized mercury in the flue gas is water-soluble and is removed. The ICR mercury data demonstrated that ionic mercury is removed effectively approaching 90% by wet FGDs. Hence, one strategy for mercury capture is to solidize all the mercury during the burning of the



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| DN | Document Number | IN | Inventor Name |
| PD | Publication Date | IC | Inventor City |
| TTL | <u>Title</u> | IS | Inventor State |
| ABST | Abstract | ICN | Inventor Country |
| ACLM | Claim(s) | GOVT | Government Interest |
| SPEC | Description/Specification | AN | Assignee Name |
| CCL | Current US Classification | AC | Assignee City |
| ICL | International Classification | AS | Assignee State |
| APT | Application Type | ACN | Assignee Country |
| APN | Application Serial | KD | Pre-Grant Publication Document Kind |

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Patent Application Publication

(19) United States

(12) Patent Application Publication (10) Pub. No.: US 2010/0105129 A1 Sanchez-Pina et al.

Apr. 29, 2010

(43) Pub. Date:

(54) BIOMASS PRODUCTION SYSTEM

Jose L. Sanchez-Pina, Los Mochis (MX); Ramon Sanchez-Pina, Los Mochis (MX)

Correspondence Address: LAMBERT & ASSOCIATES, P.L.L.C. 92 STATE STREET BOSTON, MA 02109-2004 (US)

(21) Appl. No.: 12/290,044

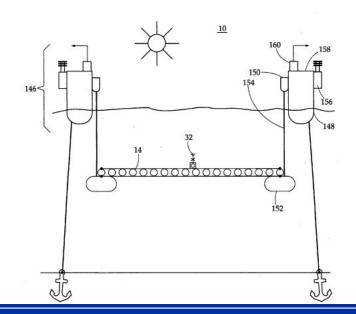
(22) Filed: Oct. 27, 2008 **Publication Classification**

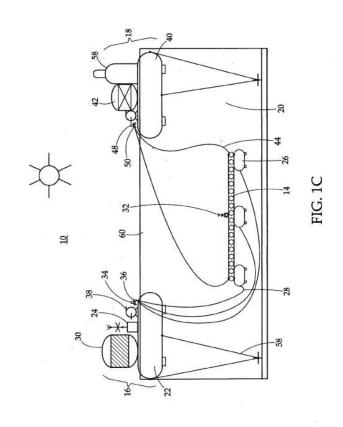
(51) Int. Cl. C12M 1/09 (2006.01)(2006.01) C12M 3/00

435/286.5: 435/292.1 (52) U.S. Cl. ..

(57) ABSTRACT

A system preferably for light irradiation, wherein the system includes a support structure, wherein the support structure is able to accommodate an array of vessels capable of receiving light; the system includes a buoyancy support system and a feeding harvesting system, wherein the buoyancy support system is in fluid and data communication with the array of vessels to regulate the amount of light introduced into the vessels within a fluid medium.





Apr. 29, 2010 Sheet 3 of 11

US 2010/0105129 A1



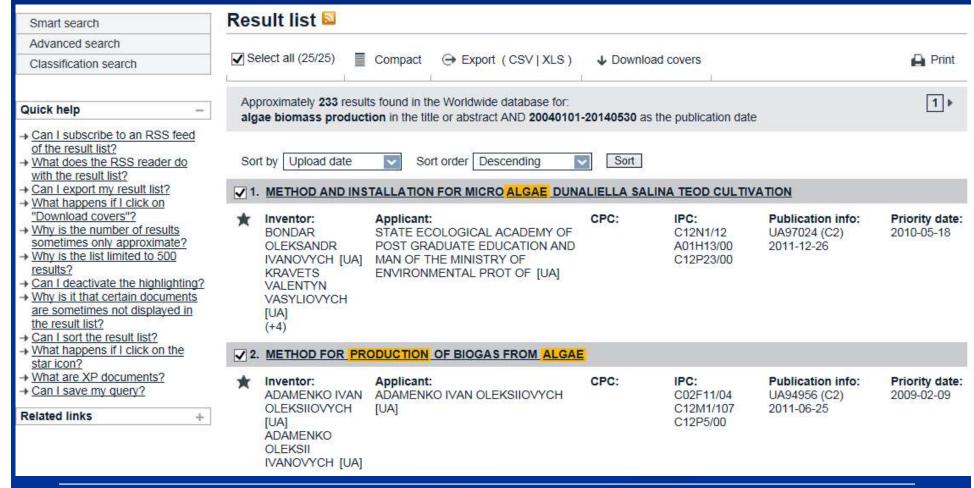
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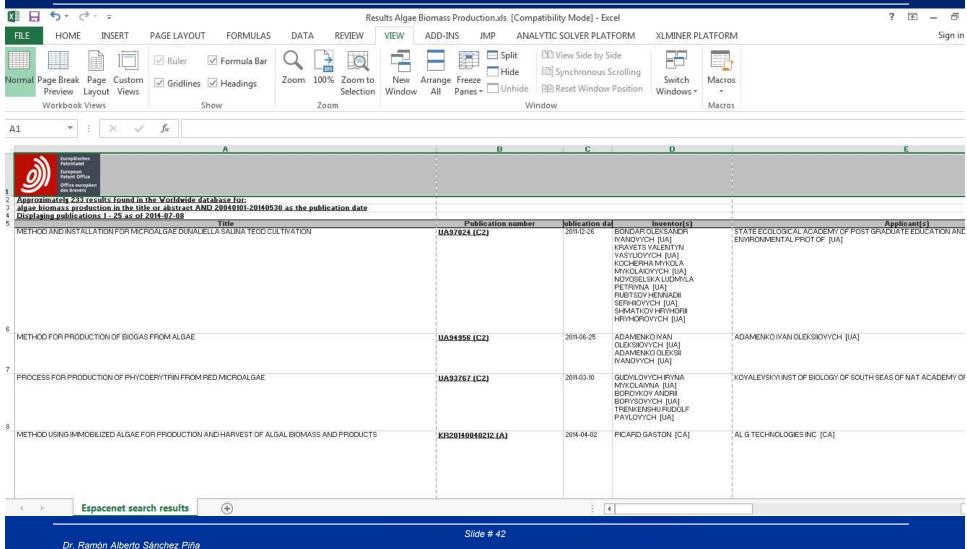
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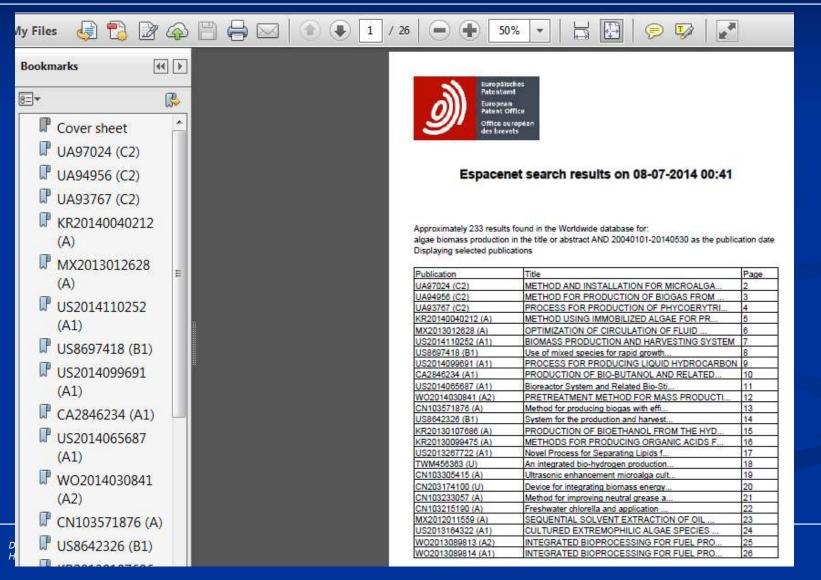
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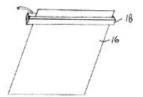
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(19) 대한민국특허청(KR) (11) 공개번호 10-2014-0040212 (12) 공개특허공보(A) (43) 공개일자 2014년04월02일 (51) 국제특허분유([nt. Cl.) C12N 1/00 (2006.01) C12N 1/12 (2006.01) 데이엘-취 제크놈보지즈 아이엠취. (21) 委集財金 10-2014-7000681 케나다 뭐백 취6에스 1이7 리바이스 뒤 드 라 브 (22) 출원일자(국제) 2012년06월13일 2125, 8340 시사체구역과 없음 (72) 10:10:24 (RS) 번역문제출일차 2014년01월09일 피카드 가스폰 케나다 캠벡 취6에스 1이7 샤르니 뷔 드 라 브리 (86) 국계총위반호 PCT/CA2012/050397 (87) 국제공개번호 #0 2012/171123 (74) tilelet 국제공개인자 2012년12월20일 리해복목위법인 61/496.171 2011년06월13일 미국(US)

전체 정구항 수 : 용 41 항

(54) 방병의 병원 조류 바이오레스의 생산 및 수거를 위한 고정화 조류의 사용 방법 및 제품

이상원류는 및 관의 공급위에 대학 전근용 제공하는 기상 환경 내의 지지체 상에서의 고전환된 조류의 성장, 및 후속 수가 및 바이오데스 가장을 위한 조성물, 용품, 장치, 방법 및 시스템이 제공된다.



Instituto Mexicano de la Propiedad Industrial



m MX 2013012628 A

(12) United States Patent

(54) SYSTEM FOR THE PRODUCTION AND HARVESTING OF ALGAE (76) Inventors: Alan W. Schaefer, Ste. Genevieve, MO (US): Brundon D. Cahot, Stc.

Genevieve, MO (US) (*) Notice: Subject to any discharger, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 559 days.

(21) Appl. No.: 12/874,751

Schaefer et al.

Related U.S. Application Data

(60) Provisional application No. 61/239,306, filed on Sep.

C12M 1/80 C12M 3/00 (2006.00) (2006.01) CI2N 1/12 A91G 7/89 (2006.01) A91H 13/00 (2006.01)

USPC 435/292.1; 47/1.4; 435/257.1; 435/283.1;

See application file for complete search history.

Feb. 4, 2014

(10) Patent No.: (45) Date of Patents

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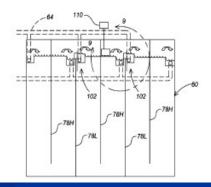
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Prinary Eurniner - Naftan Bowers Asstraw Econiner - Lydia Edwards (74) Attorney, Agent, or Firm - Grace J. Fishel

ABSTRACT

A system for the production and harvesting of algae including one or more of the following components: A turbulator for disselving carbon diexide in water to form an algae growth media, a photobiorouctor having a serpentine flow path for the algae growth media through spaced apart high and low baffles with an associated light source, a devotoring device for the algae slurry harvested from the photobioreactor, a turbulator for breaking up the cells in the algae studge coming off the devotering device, a cooker for cooking the broken up algae cells under pressure and a settling tank for separating the cooked cells into oil, spent media and biomoss fractions

16 Claims, 12 Drawing Shoets



SOLICITUD de PATENTE

| (43) Fecha de publicación: (22) Fecha de presentación: (21) Número de solicitud: | 31/01/2014 29/10/2013 2013012626 | | FOAF 5/66 to solicitud PCT: te publicación P | (2006.61) (2006.61) US 12/35250 CT: WO 2012/149214 (01/11/2012) |
|--|--|---|--|--|
| (30) Prioridad(es): 29/04/2011 US 13/ | 098,336 | | | |
| (71) Solicidente: AURORA ALGAE, INC. 3325 Investment Blvd. 94545 | Hayward California US | | | |
| (72) Inventor(es): Mehran PARSHEH 3325 Investment Blvd. Haywo Guido RADAELLI | ed California 94545 US | | | |
| (74) Representante: José F. HINOJOSA CUÉLLAF Paseo de los Tamarindos 400 DE MORELOS Distrito Feder: | -A, Piso 9 CUAJIMALP. | 4 | | |

(54) Titulo: OPTIMIZACION DE CIRCULACION DE FLUIDO EN UN ESTANQUE DE CULTIVO DE ALGAS.

(54) Title: OPTIMIZATION OF CIRCULATION OF FLUID IN AN ALGAE CULTIVATION POND.

(57) Resumen

Estanques de cultivo de algas que tienen la circulación de fluido optimizado para tales factores como consum de energia reducido, depredadores/competidores reducidos, conas muertas de flujo reducidas o eliminadas (es decir, regiones estancadas), y la producción de biomasa de algas incrementada, alí como para la poducción de biocombastibles y ofros productos a base de algas. Una primera parte inferior del estanque puede quade hajo la como cana de expansión, una parte desterior puede formar un ángulo con la primera parte inferior del estanque puede aproximadamente noventa a más de nderse hacia afuera de la primera parte inferior del estanque. La aleta en la zona de expansión puede extenderse hasta un punto por arriba de la segunda parte inferior del estanque

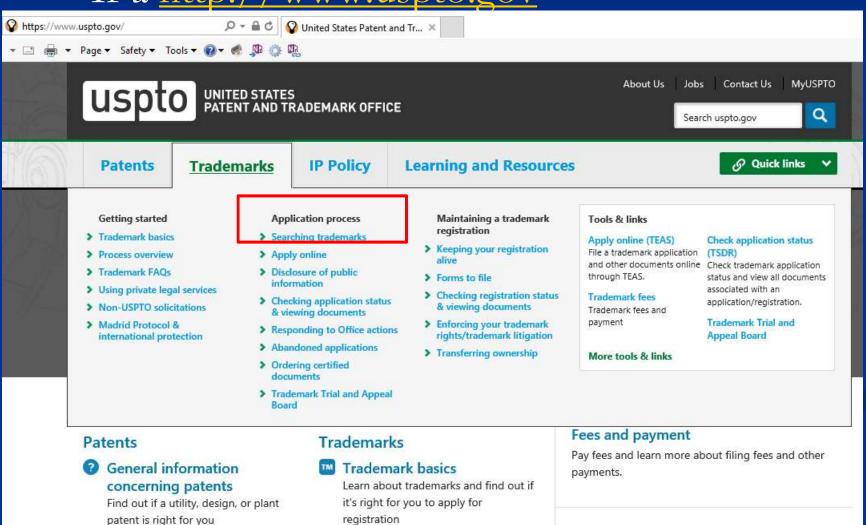
(57) Abstract

Algae cultivation ponds having the circulation of fluid optimized for such factors as decreased energy consumption decreased predators competitors, decreased or eliminated flow deadzones (i.e. stagnant regions), and increased aleae biomass production, such as for the production of biofuets and other algae-based products. A first pond bottom may underlie the expansion zone. An exterior wall may form an angle with the first pond bottom of approximately ninety to greater than one-hundred-sixty degrees. A second pond bottom adjacent to the first pond bottom may have an approximately consistent ground elevation, approximately matching a lowermost ground elevation of the first pond bottom.

Additionally, the second pond bottom may extend outward from the first pond bottom. The varie in the expansion zone may extend to a point above the second pond bottom.

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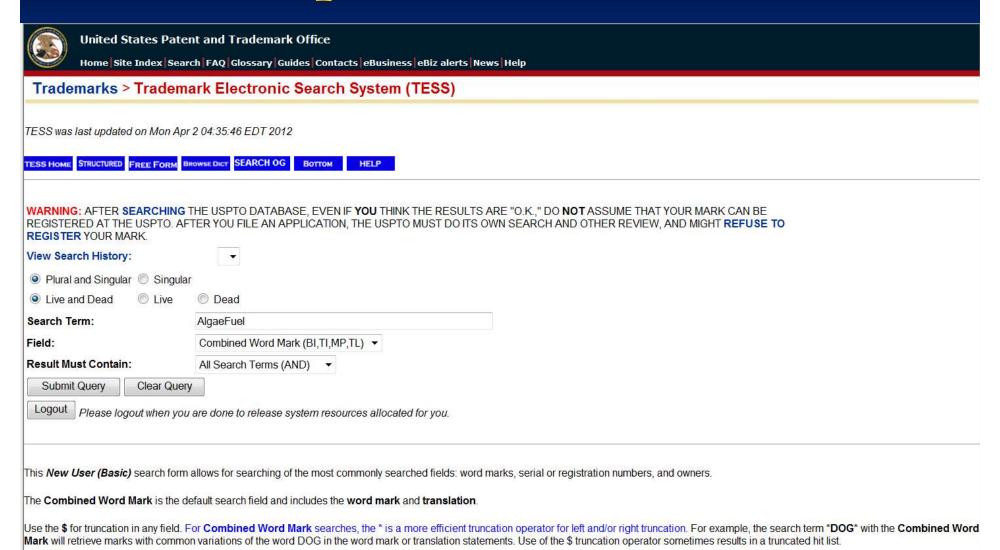
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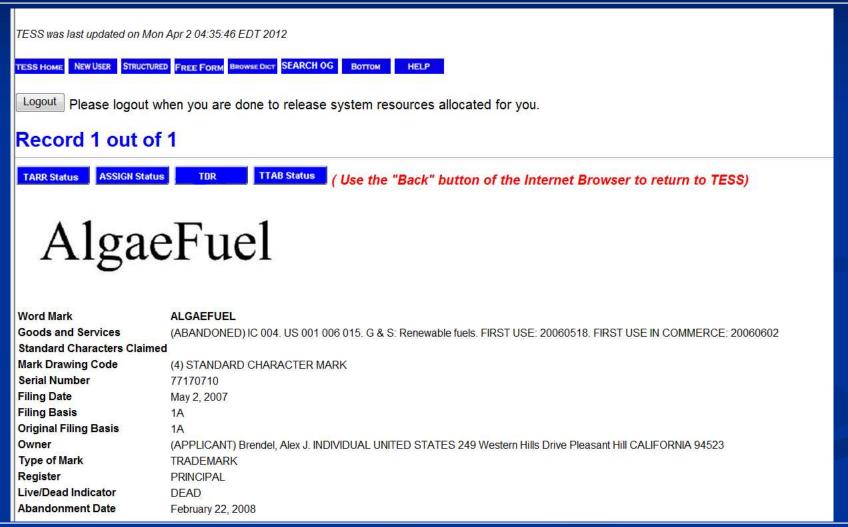
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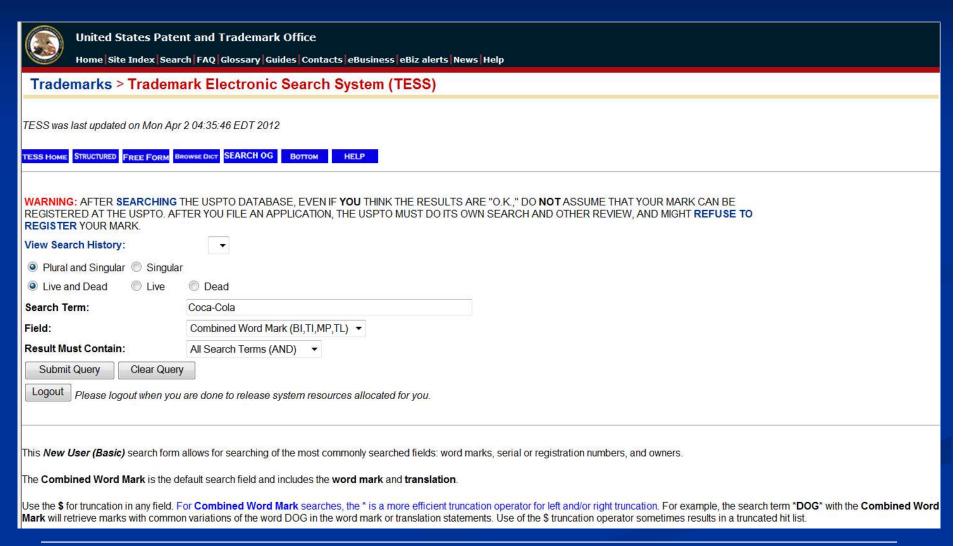
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Record 25 out of 172 OR Jump to record: Start List At: **ASSIGN Status** TTAB Status **TARR Status** (Use the "Back" button of the Internet Browser to return to TESS) COCA-COLA ZERO Word Mark COCA-COLA 7FRO Goods and Services IC 032. US 045 046 048. G & S: Beverages, namely soft drinks; syrups and concentrates for the making of the same. FIRST USE: 20050613. FIRST USE IN COMMERCE: 20050613 Standard Characters Claimed Mark Drawing Code (4) STANDARD CHARACTER MARK Serial Number 78580598 **Filing Date** March 4, 2005 Filing Basis 1A **Original Filing Basis** 1B **Published for Opposition** April 17, 2007 Owner (APPLICANT) The Coca-Cola Company CORPORATION DELAWARE One Coca-Cola Plaza Atlanta GEORGIA 30313 Attorney of Record Paula Guibault **Prior Registrations** 0238145;0238146;AND OTHERS Type of Mark TRADEMARK Register PRINCIPAL-2(F)-IN PART Live/Dead Indicator LIVE

As to "ZERO"

Distinctiveness Limitation

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Dr. Ramon Sanchez. E-mail: rsanchez@hsph.harvard.edu



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